



## INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

<b>(51) International Patent Classification <sup>5</sup> :</b> <b>G02B 3/02</b>	<b>A1</b>	<b>(11) International Publication Number:</b> <b>WO 94/14090</b> <b>(43) International Publication Date:</b> 23 June 1994 (23.06.94)
<b>(21) International Application Number:</b> PCT/US93/12203 <b>(22) International Filing Date:</b> 14 December 1993 (14.12.93)  <b>(30) Priority Data:</b> 07/991,061           15 December 1992 (15.12.92)   US 07/996,549           24 December 1992 (24.12.92)   US  <b>(71) Applicant:</b> GTE LABORATORIES INCORPORATED [US/US]; 1209 Orange Street, Wilmington, DE 19801 (US).  <b>(72) Inventor:</b> FOHL, Timothy; 681 South Street, Carlisle, MA 01741 (US).  <b>(74) Agent:</b> MONKS, Lawrence, E.; GTE Telecommunications Products and Services, 40 Sylvan Road - MS#31, Waltham, MA 02254 (US).		<b>(81) Designated States:</b> CA, JP, European patent (AT, BE, CH, DE, DK, ES, FR, GB, GR, IE, IT, LU, MC, NL, PT, SE).  <b>Published</b> <i>With international search report.</i>
<b>(54) Title:</b> WIDE ANGLE, NARROW BAND OPTICAL FILTER  <b>(57) Abstract</b> <p>The object of the invention is to provide an optical filtering system which can utilize wide angle optics and still maintain a very narrow pass band. A filtering system (100) is disclosed for receiving and bandpass filtering free space optical signals. The filtering system (100) includes a compound parabolic concentrator (110) with a small aperture for accepting the free space optical signals (115) and a larger aperture whereby the optical signal (115) exits. The compound parabolic concentrator (110) has a reflective coating on the inner surface to reflect incident optical signals (115) to produce a substantially collimated signal beam. The collimated signal is further passed through a narrow, bandpass filter (140) before detection by a photodetector device (150). In an alternative embodiment, a compound hyperbolic concentrator (310) is utilized to reflect the incident optical signals and produce a substantially collimated signal beam.</p> <div data-bbox="958 1113 1516 1932"> </div>		

**FOR THE PURPOSES OF INFORMATION ONLY**

Codes used to identify States party to the PCT on the front pages of pamphlets publishing international applications under the PCT.

AT	Austria	GB	United Kingdom	MR	Mauritania
AU	Australia	GE	Georgia	MW	Malawi
BB	Barbados	GN	Guinea	NE	Niger
BE	Belgium	GR	Greece	NL	Netherlands
BF	Burkina Faso	HU	Hungary	NO	Norway
BG	Bulgaria	IE	Ireland	NZ	New Zealand
BJ	Benin	IT	Italy	PL	Poland
BR	Brazil	JP	Japan	PT	Portugal
BY	Belarus	KE	Kenya	RO	Romania
CA	Canada	KG	Kyrgyzstan	RU	Russian Federation
CF	Central African Republic	KP	Democratic People's Republic of Korea	SD	Sudan
CG	Congo	KR	Republic of Korea	SE	Sweden
CH	Switzerland	KZ	Kazakhstan	SI	Slovenia
CI	Côte d'Ivoire	LI	Liechtenstein	SK	Slovakia
CM	Cameroon	LK	Sri Lanka	SN	Senegal
CN	China	LU	Luxembourg	TD	Chad
CS	Czechoslovakia	LV	Latvia	TG	Togo
CZ	Czech Republic	MC	Monaco	TJ	Tajikistan
DE	Germany	MD	Republic of Moldova	TT	Trinidad and Tobago
DK	Denmark	MG	Madagascar	UA	Ukraine
ES	Spain	ML	Mali	US	United States of America
FI	Finland	MN	Mongolia	UZ	Uzbekistan
FR	France			VN	Viet Nam
GA	Gabon				

WIDE ANGLE, NARROW BAND OPTICAL FILTER

## Technical Field

The instant invention relates generally to optical  
5 filters and more particularly to apparatus which can be  
used to build optical systems with very narrow band  
transmission.

## Background Art

10 Often it is desirable to block light or any other  
optical band radiation from reaching a detector with the  
exception of radiation within a specific wavelength band.  
Narrow band optical systems have been developed for a wide  
variety of applications for many years. The usual  
15 objective is to isolate an optical signal of a specific  
wavelength in the presence of a large flux of noise i.e.  
optical radiation at other wavelengths. A better signal to  
noise ratio can be derived from the detector if the signal  
is within a narrow band of the optical spectrum. Noise is  
20 caused by background light outside the band of the signal  
and such filters typically find use in wireless  
communication applications as described by Barry, et al.  
in "High-Speed Nondirective Optic Communication for  
Wireless Networks", IEEE Network Magazine, November 1991.

25 In conventional filtering systems, the absorption of  
light at specific wavelengths is sometimes used as a means  
of filtering. However such filters are usually not capable  
of isolating a narrow passband, and they tend to be lossy  
at the desired band.

30 In a further approach, filters composed of layers of  
thin dielectric films consisting of materials with widely  
differing refractive indices have been utilized. Such  
filters are known as interference filters and are capable  
of isolating quite narrow passbands with relatively high  
35 transmission at the desired band. Interference filters,

1923-369C.PCTI

however, have the characteristic that the passband shifts as the angle the light ray makes with respect to the surface of the filter varies. This characteristic is a disadvantage in filtered optical systems which require  
5 wide angle reception again as described in Barry, et al., supra.

A filtering system which provides for wide angle reception is described by Martin and Fohl in U.S. Patent 5,124,859. Although this filter is a clear advance over  
10 the prior art, it can only operate at wavelengths for which suitable atomic transitions exist.

It is thus desirable to provide an optical filtering system that has a wide angle of acceptance but maintains the narrow passband of a interference filter normal to a  
15 well collimated beam. It is further desirable that such a filtering system be amenable to a simple and compact implementation.

#### Disclosure of the Invention

20 The above and other objects and advantages are achieved in one aspect of the invention using a compound parabolic concentrator for reception of free space optical signals preferably in the infrared band of the electro-  
magnetic spectrum. The compound parabolic concentrator has  
25 a first aperture for accepting the free space optical signals. The angle of acceptance of the free space optical signals is defined by this aperture. The received optical signals pass through the compound parabolic concentrator causing them to be substantially collimated. The optical  
30 signals exit the compound parabolic concentrator at a second aperture of the device which is larger than the first before they are input to an interference filter for bandpass filtering of the signals. The filtered signal may be concentrated using a second compound parabolic  
35 concentrator before being presented to a photodetector for converting the optical signal to an electrical signal.

-3-

Other types of filters can be based on holographs or gratings, but these are not as efficient in that they lose resolution if the angle of light varies over a wide angle.

In another embodiment of the invention, a hyperbolic  
5 concentrator is utilized for receiving and collimating the free space optical signal.

#### Brief Description of the Drawings

FIG. 1 is a cross sectional view of a filter system  
10 utilized in receiving free space optical signals in accordance with one embodiment of the instant invention.

FIG. 2 is a graph of a transmission-angle curve for a compound parabolic concentrator.

FIG. 3 is a cross sectional view of a filter system  
15 utilized in receiving free space optical signals in accordance with one embodiment of the instant invention and using a second compound parabolic concentrator for concentrating the input signal to a photodetector.

#### 20 Best Mode for Carrying Out the Invention

One embodiment of the invention is depicted in FIG. 1 which is a cross section of the instant filtering system 100 for receiving free space optical signals, preferably in the infrared band of the electromagnetic spectrum.  
25 However, other optical signals for example signals in the the visible and ultraviolet spectrum are within the scope of the invention. In this embodiment radiation, both the signal and background noise enters the device as rays through the small end of a compound parabolic concentrator 110. A compound parabolic concentrator consists of a  
30 reflective surface defined by sweeping a parabola around a line or axis in space. Similarly, a compound hyperbolic concentrator is defined by sweeping a hyperbola around a line or axis in space. The surfaces so defined have a  
35

-4-

small aperture for accepting the free space optical signal and a larger aperture for the exiting signal which has been substantially collimated by the geometry of the device. The details of the geometry of these concentrators and other types which use combinations of refraction and reflection are given in High Collection Nonimaging Optics by Welford and Winston. The essential feature of all these devices is that they exchange decreased angular spread of the beam for enlarged beam cross section. Used in the opposite sense these devices exchange smaller beam size for larger spread angles - hence the term concentrators.

As shown in FIG. 1, an input optical signal 115 enters the compound parabolic concentrator through the small aperture and is reflected off the internal side walls of the device. As a result of the reflection of the optical signal 115, the signal exits the compound parabolic concentrator at the large aperture substantially collimated before passing to photodetector 150. For a concentrator with a small aperture of area  $H$  for receiving a free space optical signal at a maximum angle  $A$  and a large aperture  $K$  for exiting the signal at a maximum exit angle of  $B$ , the product of  $H \times A$  is substantially equal to the product of  $K \times B$ . Optical signal Interference filter 140 is of conventional design, and is known by those skilled in the art.

The behavior of an interference filter 140 as the optical rays enter the filter away from the normal is described in Optical Filters and Coatings by Corion Corporation of Hopkinton, Massachusetts (October 1988). Consequently, an estimate of the effective band pass of the filtering 100 system can be derived. With a very narrow passband for the interference filter 140, the system passband will be given by the shift in transmission wavelength at the maximum angle of the cone of rays,  $B$ . The percentage shift in pass wavelength is given by:

-5-

$$\text{Percentage wavelength shift} = \frac{100(n_s^2 - \sin^2 B)^{0.5}}{n_s}$$

5 where  $n_s$  is an average value of the index of refraction of the interference filter 140, and B is the angle between the beam and the normal to the plane of the filter. As an example, with the average index as 2.0 and an acceptance angle of 10 degrees, the shift is approximately 0.4  
 10 percent. With the pass band of the filter centered at 800 nm, the pass band of the system is approximately 3.2 nm. Accordingly, a filtering system with an arbitrarily wide viewing angle can be shown to have a passband only a few nanometers wide.

15 FIG. 2 is a transmission-angle curve for a compound parabolic concentrator with an angle of exit of B. In this example an exit angle of sixteen degrees is the maximum exit angle. The compound parabolic concentrator comes close to being an ideal concentrator, and has the  
 20 advantages of being a very practical design and easy to make for all wavelengths since it depends on reflection rather than refraction.

The above achieves the objects of the invention. However, it does this at the cost of reducing the signal  
 25 as well as the noise. The signal attenuation can be counteracted by increasing the surface area of the ends of the fibers and the detector. In some applications where there are limits on detector area for example because of frequency response requirements or cost, a second compound  
 30 parabolic concentrator 310 can be utilized between the interference filter and the detector to concentrate the optical rays on photodetector 150 as shown in FIG. 3. The second compound parabolic concentrator is used in a configuration which is opposite the first compound  
 35 parabolic concentrator. The rays from filter 140 enter the compound parabolic concentrator 310 substantially

-6-

collimated and are focused through reflection off the side walls of the device onto photodetector 150. Concentration increases the angle of the rays relative to the optical axis of the system. The product of this angle and the area  
5 through which the bundle of rays flow, called the etendue, is constant. However, the detector typically accepts energy over a wide angle with the spread angle emerging from the filter being small in comparison. Thus even in  
10 systems where detector area is a limiting factor on signal level, the instant filtering system allows high rejection of background noise without sacrificing much signal.

While there has been shown and described what is at present considered the preferred embodiment of the invention it will be obvious to those skilled in the art  
15 that various changes and modifications may be made therein without departing from the invention as defined by the appended claims.

20

25

30

35



## Claims:

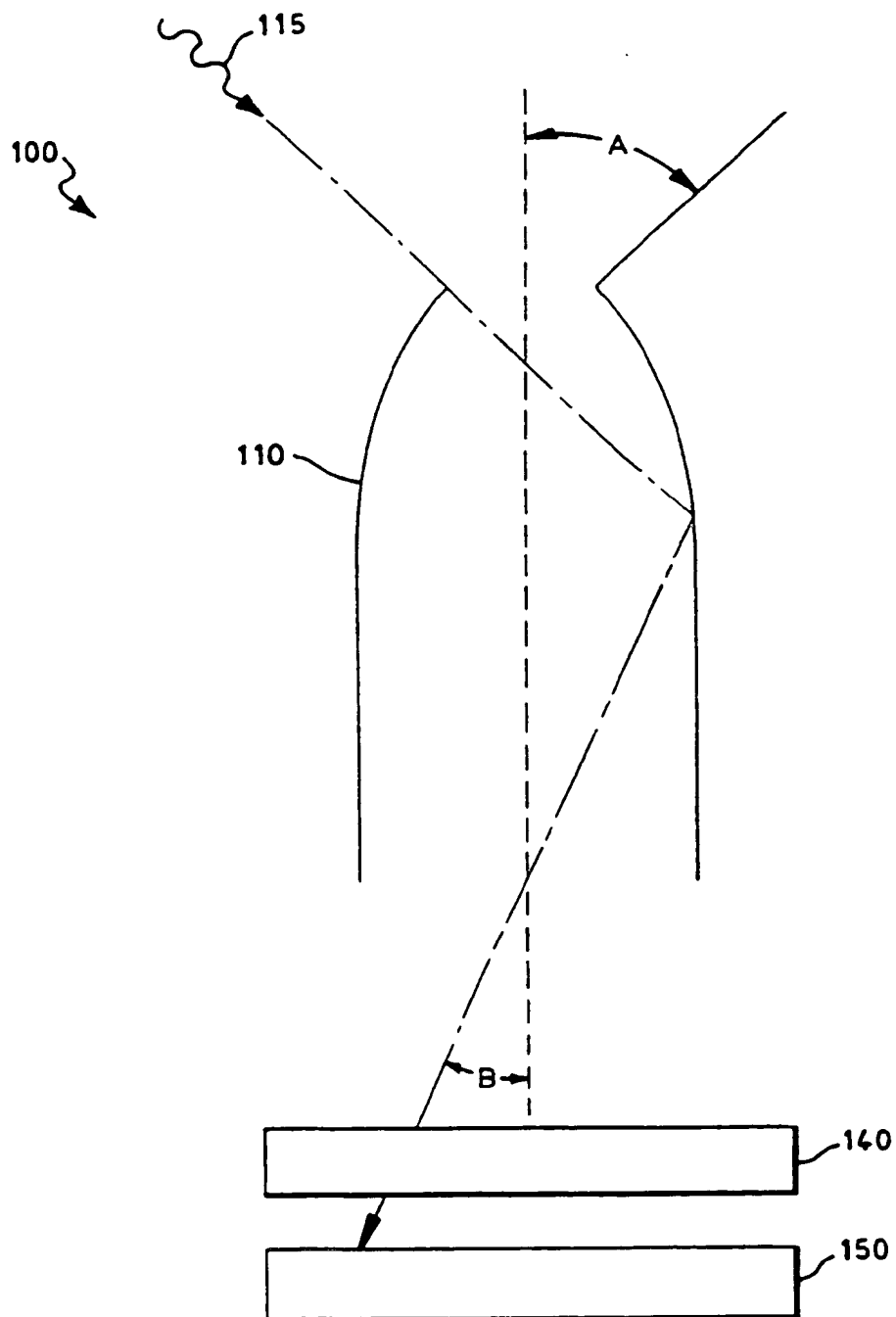
1. A filtering system for receiving a free space optical signal separated from background optical noise comprising:
- 5 a compound hyperbolic concentrator means having a first aperture of area H for for receiving said optical signal at a maximum angle A and passing said free space optical signal therethrough, exiting at a second aperture of area K with a
- 10 maximum exit angle of B;
- an filter means coupled to said compound parabolic concentrator means for rejecting said background optical noise and transmitting said optical signal exiting from said compound parabolic
- 15 concentrator means;
- a photodetector means for detecting said transmitted optical signal of the filter means.

20

25

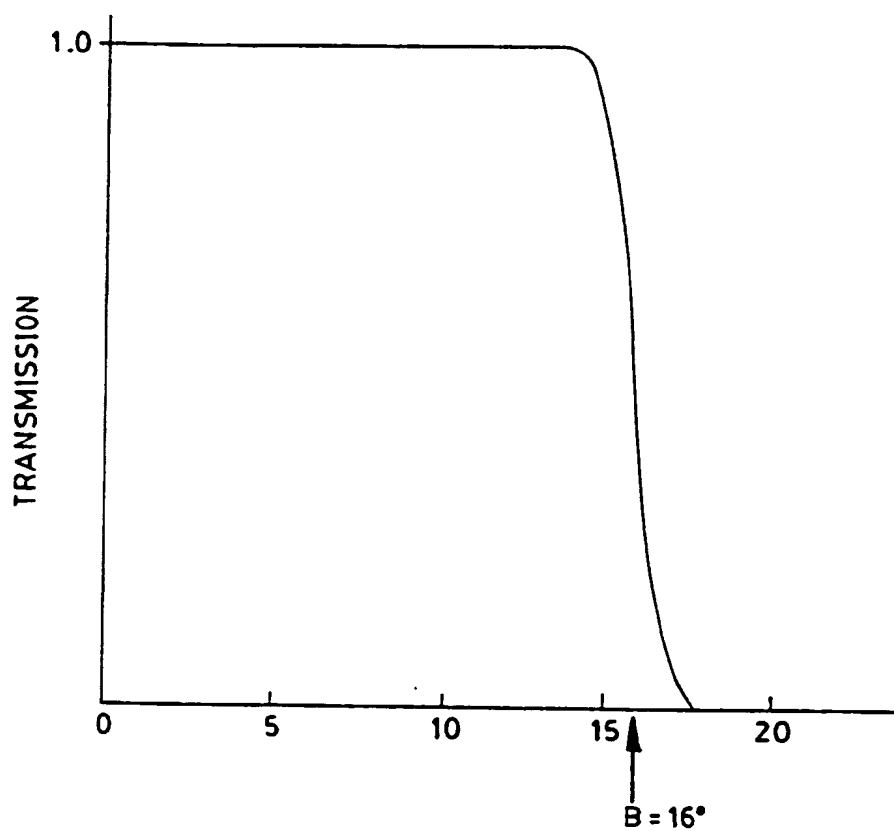
30

35

**FIG. 1**

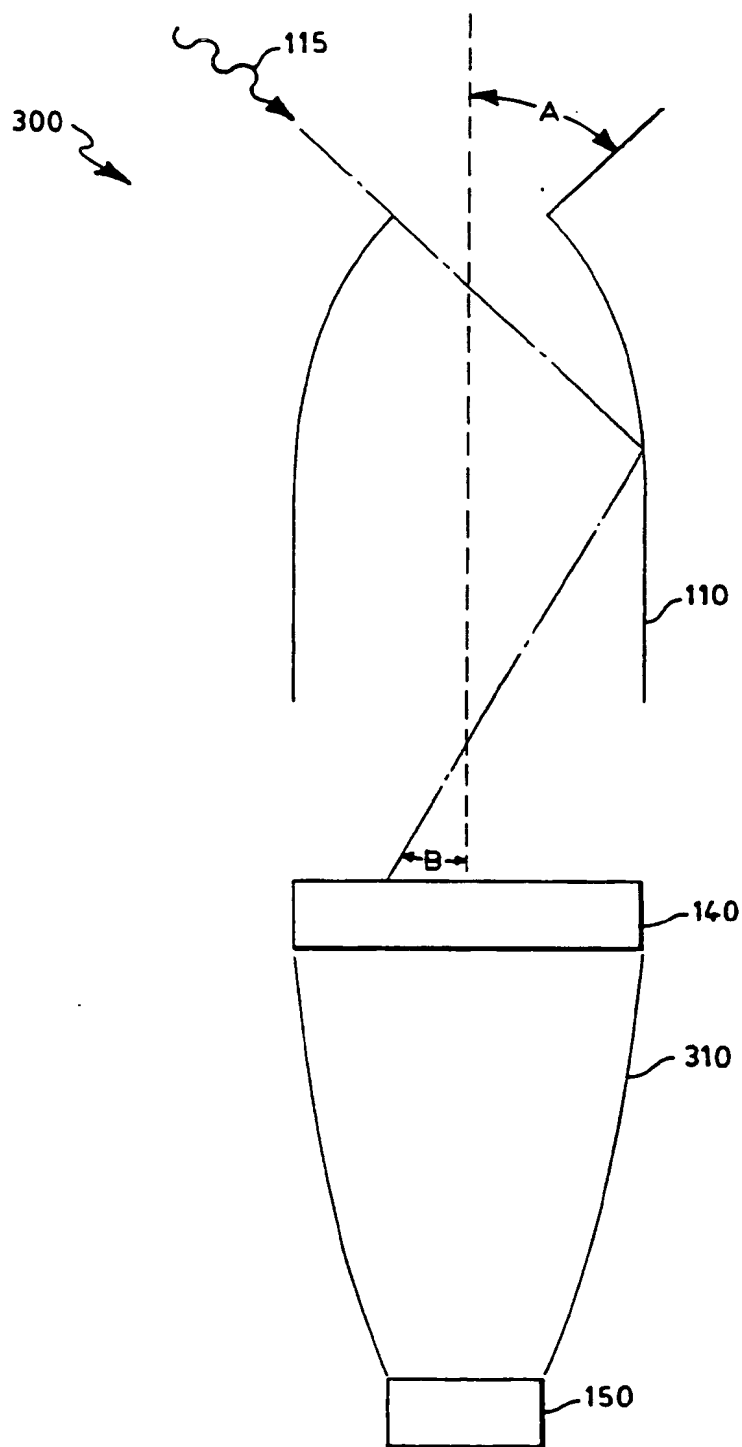
SUBSTITUTE SHEET (RULE 26)

2 / 3

*FIG. 2*

SUBSTITUTE SHEET (RULE 26)

3/3

**FIG. 3**

SUBSTITUTE SHEET (RULE 26)

# INTERNATIONAL SEARCH REPORT

International application No.  
PCT/US93/12203

## A. CLASSIFICATION OF SUBJECT MATTER

IPC(5) : G02B 3/02

US CL : 359/708, 712, 738

According to International Patent Classification (IPC) or to both national classification and IPC

## B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

U.S. : 359/708, 712, 738, 709, 739

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

## C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	Ruda, Mitchell C., "How and when to use a nonimaging concentrator," SPIE, August, 1983, Int. Conf. Hew Imaging concentrators, pp. 51-58, see Figs. 6 and 7.	1

☐ Further documents are listed in the continuation of Box C. ☐ See patent family annex.

* Special categories of cited documents:	* T	later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention
* A* document defining the general state of the art which is not considered to be part of particular relevance	* X*	document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone
* B* earlier document published on or after the international filing date	* Y*	document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art
* L* document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)	* A*	document member of the same patent family
* O* document referring to an oral disclosure, use, exhibition or other means		
* P* document published prior to the international filing date but later than the priority date claimed		

Date of the actual completion of the international search 18 February 1994	Date of mailing of the international search report 24 FEB 1994
Name and mailing address of the ISA/US Commissioner of Patents and Trademarks Box PCT Washington, D.C. 20231 Facsimile No. NOT APPLICABLE	Authorized officer for THOMAS ROBBINS <i>Smiller</i> Telephone No. (703) 305-3792

Form PCT/ISA/210 (second sheet)(July 1992)\*

**This Page is Inserted by IFW Indexing and Scanning  
Operations and is not part of the Official Record**

**BEST AVAILABLE IMAGES**

Defective images within this document are accurate representations of the original documents submitted by the applicant.

Defects in the images include but are not limited to the items checked:

- ☒ **BLACK BORDERS**
- ☐ **IMAGE CUT OFF AT TOP, BOTTOM OR SIDES**
- ☐ **FADED TEXT OR DRAWING**
- ☐ **BLURRED OR ILLEGIBLE TEXT OR DRAWING**
- ☐ **SKEWED/SLANTED IMAGES**
- ☐ **COLOR OR BLACK AND WHITE PHOTOGRAPHS**
- ☐ **GRAY SCALE DOCUMENTS**
- ☐ **LINES OR MARKS ON ORIGINAL DOCUMENT**
- ☐ **REFERENCE(S) OR EXHIBIT(S) SUBMITTED ARE POOR QUALITY**
- ☐ **OTHER:** \_\_\_\_\_

**IMAGES ARE BEST AVAILABLE COPY.**

**As rescanning these documents will not correct the image problems checked, please do not report these problems to the IFW Image Problem Mailbox.**